

Nanosecond Laser Damage Resistance of Differently Prepared Semi-finished Parts of Optical Multimode Fibers

G. Mann¹, J. Vogel¹, R. Preuss¹
P. Vaziri¹, M. Zoheidi², M. Eberstein¹, J. Krüger¹

¹ Federal Institute for Materials Research and Testing, Unter den Eichen 87, D-12205 Berlin, Germany

² FiberTech GmbH, Nalepastrasse 171, D-12459 Berlin, Germany

Introduction

- Optical multimode fibers are applied in fields like automotive, defense, aviation, medicine and biotechnology
- High power applications (fiber lasers, laser light cable) are of increasing interest
- Besides geometrical parameters and absorption behavior of fibers the laser damage threshold is a major aspect

Problem

Laser-induced damage threshold (LIDT) can limit the performance of complex optical systems with respect to beam quality and transmissible power

Question:

Does the pulling process (pulling temperature, cooling rate, mechanical stress) and the polishing of fiber end faces influence the LIDT?

Experimental

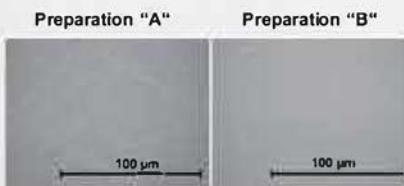
Specimens:

- Material: SiO₂ glass (F300, Heraeus)
- Multimode fiber preform
- Cylindrical samples: 20 mm diameter and 10 mm thick
- Transformation temperature (F300): 1070 °C

Surface preparation:

According to sequences "A" and "B"

Surface Preparation Steps	"A"	"B"
Grinding with abrasive grains with grain diameters down to $\approx 15 \mu\text{m}$	*	*
Polishing with Ce ₂ O ₃ suspension with Ce ₂ O ₃ grain diameters of 3 μm		*
Polishing with diamond suspension with diamond grain diameters of 3 μm	*	*
Polishing with diamond suspension with diamond grain diameters of 1 μm	*	*
Polishing with diamond suspension with diamond grain diameters of 0.25 μm	*	*



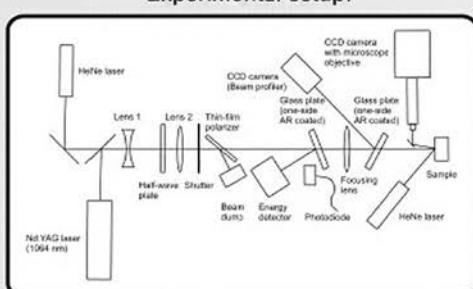
Thermal treatment:

- Tempered at 1100 °C, 1300 °C and 1500 °C for 15 min.
- Cooling rates: 10 K/min (oven) and 10⁵ K/min (quenched in air)

Laser setup:

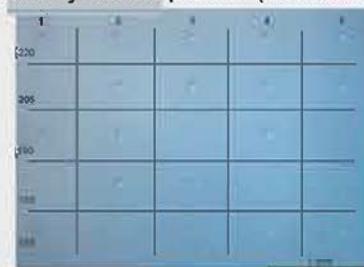
- Nd:YAG laser
- 1064 nm, 12 mJ, 10 Hz
- Gaussian beam profile
- 2w = 50 ± 2 μm
- M² = 1.6
- Precision of absolute LIDT value: 25%
- Maximum laser fluence: $F_0 = \frac{2E_0}{\pi w^2}$ (pulse energy)

Experimental setup:



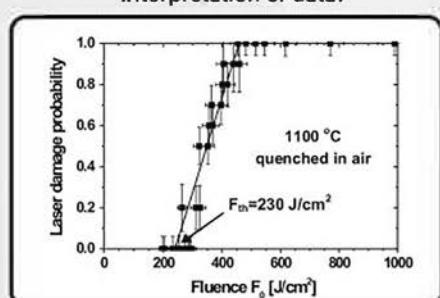
According to standard ISO 11254-1/2:
Part 1: 1-on-1 Test / Part 2: S-on-1 Test

Array of laser induced damage sites on a cylindrical preform (1-on-1 test):



top: consecutive numbers of damage sites
left: relative laser power

Interpretation of data:



Damage probability vs. maximum laser fluence

Results

Maximum temperature [°C]	Surface preparation	F _{th} cooling rate 10 Kmin ⁻¹ [$\mu\text{J}/\text{cm}^2$]	F _{th} cooling rate 10 ⁵ Kmin ⁻¹ [$\mu\text{J}/\text{cm}^2$]
20	B	220	-
1100	B	230	230
1300	B	250	350
1500	B	320	250
1600	A	130	-

Damage threshold fluences F_{th} for cylindrical preforms with different thermal history and varying surface preparation (1-on-1)

Maximum temperature [°C]	Surface preparation	F _{th} 1-on-1 [$\mu\text{J}/\text{cm}^2$]	F _{th} 100-on-1 [$\mu\text{J}/\text{cm}^2$]
20	B	220	220
1100	B	230	210
1300	B	250	270
1500	B	320	230

Damage threshold fluences F_{th} for cylindrical preforms with different thermal history
Comparison between (1-on-1) and (100-on-1) laser treatment

Conclusions

- LIDT values between 150 J/cm² and 350 J/cm² (1064 nm, 15 ns, unseeded)
- An insufficient polishing procedure decreases the damage resistance significantly
- A thermal pre-treatment enhances the damage threshold
- A multi pulse impact results in lower thresholds compared to the single pulse illumination (incubation effect)

Funding

Financial support by the federal state Berlin in the framework of the ProFIT program partly financed by the European Union (EFRE) is gratefully acknowledged.

